# **RFbeam Microwave GmbH**

### K-MC2 RADAR TRANSCEIVER

Replaced by K-MC3 Datasheet

### Features

- 24 GHz short range transceiver
- 90MHz sweep FM input
- High sensitivity, integrated RF/IF amplifier
- Dual 62 patch narrow beam antenna
- Buffered, gain adjustable I/Q IF outputs
- Additional DC IF outputs
- Beam aperture 25°/7°
- RSW Rapid Sleep Wakeup
- Extremely compact:138x65x6 mm<sup>3</sup> construction



- Traffic supervision and counting
- Object speed measurement systems
- Ranging and distance detection
- Industrial sensors

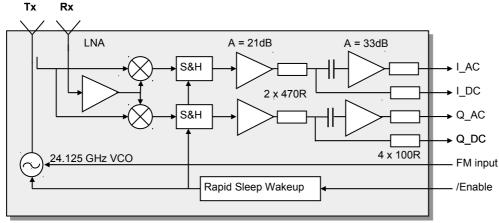
### Description

K-MC2 is a 124 patch doppler module with an asymmetrical narrow beam for long distance sensors. It is ideally suited for traffic supervision.

This module includes a RF low noise amplifier and two IF preamplifiers for both I and Q channels. The need for external analogue electronics will be significantly reduced by this feature. For special signal condition applications, an additional buffered Mixer DC output is provided. This greatly improves flexibility in multistep FSK ranging applications. The unique "RSW" *R*apid Sleep *W*akeup function with <7us wakeup time makes this module ideal for battery operated equipment. Typical duty cycle in RWS mode may be < 1% with full movement detection capability by sampling the IF signals.

An extremely slim construction with only 6mm depth gives you maximum flexibility in your equipment design.

A powerful starterkit with signal conditioning and visualization is also available. (see <u>www.rfbeam.ch Download Section</u>)



### Blockdiagram

Fig. 1: K-MC2 Blockdiagram



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# Characteristics

Parameter	Conditions / Notes	Symbol	Min	Тур	Max	Unit
Operating conditions						
Supply voltage		V <sub>cc</sub>	4.75	5.0	5.25	V
Supply current	Module enabled (Pin 1 = $V_{L}$ )	I <sub>cc</sub>		80	100	mA
	Module RSW mode (Pin 1 = V <sub>IH</sub> )			5	7	mA
VCO input voltage		U <sub>vco</sub>	0		5.0	V
VCO pin resistance	Internal pulldown 10k	R <sub>vco</sub>		10k		Ω
Operating temperature		Top	-20		+80	°C
Storage temperature		T <sub>st</sub>	-20		+80	°C
ower down/Enable						
Module power down	Input tied high with pullup 10k	VIH	V <sub>cc</sub> -0.7		V <sub>cc</sub> + 0.3	V
Module enable		VIL	-0.2		2	V
Minimum enable time	Sample&Hold capacitor charged	ton	7			μs
Maximum hold time	S&H error <10%	t <sub>off</sub>			2	ms
ransmitter						
Transmitter frequency	U <sub>vco</sub> = 2V, T <sub>amb</sub> =-20°C +60°C	f <sub>TX</sub>	24.050	24.150	24.250	GHz
Frequency drift vs temp.	V <sub>cc</sub> =5.0V, -20°C +60°C <sup>Note 1</sup>	$\Delta f_{TX}$		-1.0		MHz/°
Frequency tuning range		$\Delta f_{vco}$		89		MHz
VCO sensitivity		Svco		22		MHz/V
VCO Modulation Bandwidth	∆f=20MHz	B <sub>vco</sub>		3		MHz
Output power	EIRP	P <sub>TX</sub>	+16	+19	+20	dBm
Output power deviation	Full VCO tuning range	$\Delta P_{TX}$			+/- 1	dBm
Spurious emission	According to ETSI 300 440	P <sub>spur</sub>			-30	dBm
eceiver						
Antenna gain	F <sub>TX</sub> =24.125GHz Note 2	G <sub>Ant</sub>		21		dBi
LNA gain	F <sub>RX</sub> =24.125GHz	GLNA		16		dB
Mixer Conversion loss	f <sub>i</sub> =500Hz	D <sub>mixer</sub>		-6		dB
Receiver sensitivity	f <sub>IF</sub> =500Hz, B=1kHz, S/N=6dB	P <sub>RX</sub>		-126		dBm
Overall sensitivity	f <sub>IF</sub> =500Hz, B=1kHz, S/N=6dB	Dsystem		-145		dBc
- output						
IF output impedance	_AC outputs	R <sub>IF_AC</sub>		100		Ω
	_DC outputs	R <sub>IF_DC</sub>		570		Ω
IF Amplifier gain	_AC outputs	GIF_AC		54		dB
	_DC outputs	G <sub>IF_DC</sub>		21		dB
I/Q amplitude balance	f <sub>IF</sub> =500Hz, U <sub>IF</sub> =100mV <sub>pp</sub> (_AC outputs)	$\Delta U_{IF}$		3		dB
I/Q phase shift	f <sub>IF</sub> =500Hz, U <sub>IF</sub> =100mV <sub>pp</sub> (_AC outputs)	φ	80	90	100	0
IF frequency range	-3dB Bandwidth (_AC outputs)	f <sub>IF_AC</sub>	40		15k	Hz
	-3dB Bandwidth (_DC outputs)	f <sub>IF_DC</sub>	0		300	kHz
IF noise voltage	f <sub>IF</sub> =500Hz	UIFnoise		22		μV/√Hz
	f <sub>IF</sub> =500Hz	UIFnoise		-93		dBV/H
IF output offset voltage	V <sub>cc</sub> = 5V, _AC outputs	U <sub>os_AC</sub>	2.0	2.5	3.0	V
	no object in range,VCO pin open,_DC outputs	U <sub>os_DC</sub>	0.5	2.5	4.5	V
Supply rejection	Rejection supply pins to _AC outputs, 500Hz	D <sub>supply</sub>		-24	-	dB

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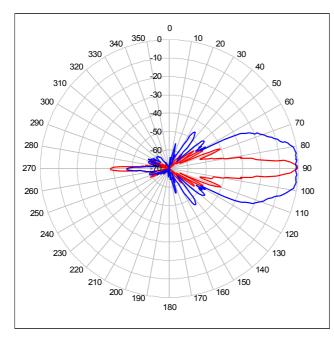
Parameter	Conditions / Notes	Symbol	Min Typ M	ax Unit
Antenna				
Horizontal -3dB beamwidth	E-Plane	W <sub>o</sub>	7	٥
Vertical -3dB beamwidth	H-Plane	W <sub>e</sub>	25	٥
Horiz. sidelobe suppression		D <sub>φ</sub>	-20	dB
Vert. sidelobe suppression		D <sub>e</sub>	-18	dB
Body				
Outline Dimensions	connector left unconnected		138x65x6	mm <sup>3</sup>
Weight			102	g
Connector	Module side: AMP X-338069-8		8	pins

Note 1 Transmit frequency stays within 24.050 to 24.250GHz over the specified temperature range when the VCO pin is set to 2VDC

Note 2 Theoretical value, given by design

#### Antenna System Diagram

This diagram shows module sensitivity (output voltage) in both azimuth and elevation directions. It incorporates the transmitter and receiver antenna characteristics.



Azimuth 7°, Elevation 25° At IF output voltage -6dB (corresponds to -3dB Tx power)

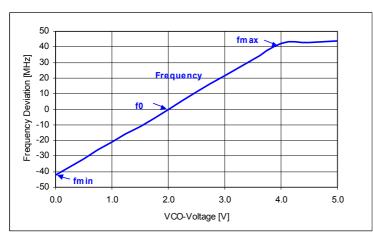
#### Fig. 2: Anntenna system diagram

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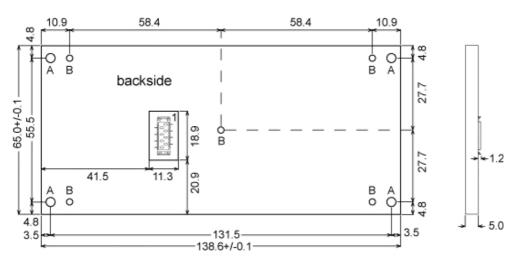
#### **FM Characteristics**





#### **Pin Configuration**

Pin	Description	Typical Value	
1	/Enable	GND: module active	
2	VCC	5V supply	
3	GND	0V supply	
4	IF output Q_AC	high gain output	
5	IF output I_AC	high gain output	
6	VCO in	$2.0V = f_0$	
7	IF output I_DC	low gain output	
8	IF output Q DC	Low gain output	



### **Outline Dimensions**

All Dimensions in mm

A 4x bore hole 3.5mm Module mounting B 5x bore hole 2.3 +/-0.03 mm PCB mounting All values given are typical unless otherwise specified.

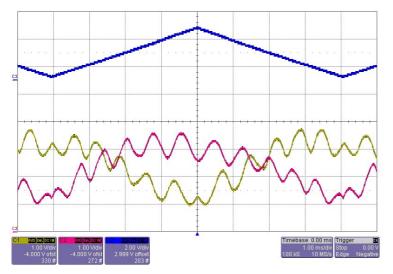
#### Fig. 4: Mechanical dimensions

### **Application Notes**

#### **Using VCO and Internal IF Amplifier**

The IF amplifier provides two outputs per channel according to Fig. 1. These outputs are designed for different requirements in processing radar signals. Both I (imaginary) and Q (real) mixer signals are available. The I and Q signals are phase shifted by  $+90^{\circ}$  or  $-90^{\circ}$ , depending on the moving direction of objects in range.

FMCW generates an output signal even without an object in range because of the finite isolation between transmitter and receiver path. This effect is called self-mixing and leads to a DC signal that depends on the carrier frequency. Using FMCW, these signals move and may overdrive the 2<sup>nd</sup> stage (x\_AC outputs) of the IF amp under certain circumstances.



Triangle VCO Voltage with A=3.8Vpp and f=125Hz. Resulting transmit frequency deviation of approx. 100MHz

I\_AC and Q\_AC outputs show a low frequency caused by local carrier feedthrough.

The superposed higher frequency with 1.25kHz is caused by a target. The peak-peak amplitude of 2.8Vpp

is no problem, because the  $x\_AC$  outputs are limited at 4.5Vpp approx.

#### Fig. 5: x\_AC Output FMCW signals with triangle VCO and df = 100MHz

#### I\_AC and Q\_AC High Gain Outputs

These outputs provide high gain/low noise signals generated by doppler effects or FMCW. They directly can drive ADC input stages of microprocessors or DSPs. Even with 10Bit of resolution only, sensitive and relatively long range Doppler detections are possible. The outputs cover a frequency range of 40Hz ... 15kHz.

However, these outputs may saturate and clip because of too high input signals. In these cases you may use the x\_DC outputs described below.

There is also a possibility to adjust output levels by using a resistor at the x\_DC outputs. (see chapter Adjusting IF Gain).

#### I\_DC and Q\_DC Low Gain Outputs

The low gain DC outputs (I\_DC and Q\_DC) hardly enter into a saturation state and may be used in cases, where the high gain outputs (I\_AC and Q\_AC) are clipped because of high input signals. Saturation and clipping typically arise in conjunction with FMCW and may be caused by objects nearby the sensor, non-compensated radoms etc.

These outputs carry more signal information than the x\_AC outputs because of their bandwidth ranging from DC to 300kHz. Using ADCs with resolutions of 12Bits and more and processing with DSP processors allow versatile and flexible radar applications.

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#### Adjusting IF Gain

If there is a risk of overdriving the  $2^{nd}$  amplifier, you may use the low gain x\_DC outputs or attenuate the input signals of the  $2^{nd}$  stage amp.

Gain of the 2<sup>nd</sup> stage amplifier may be lowered by adding an external resistor at pins I\_DC and Q\_DC connected to GND. Please refer to Fig. 1: K-MC2 Blockdiagram to understand the resistive attenuator.

 $2^{nd}$  stage gain A<sub>R</sub> may be adjusted between 18dB and 33dB resp. attenuated by max. 15dB.

Without additional Resistor: $A_R = 33dB = 45$ resulting total IF gain: 54dB = 500With short circuit at x\_DC to ground $A_R = 18dB = 8$ resulting total IF gain: 39dB = 89

$$A_R = 45/(1 + \frac{470}{100 + Rx})$$
 or  $Rx = \frac{470}{(45/A_R) - 1} - 100$ 

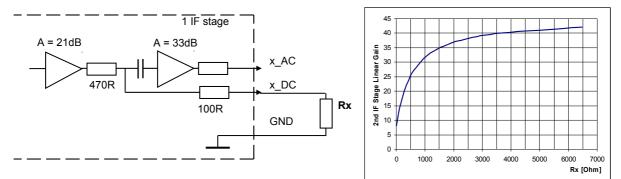


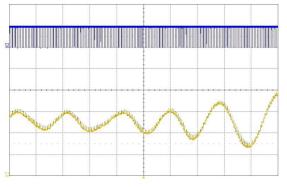
Fig. 6: Attenuating xAC outputs via x\_DC pins

#### Rapid Sleep Wakeup (RSW)

RFbeam's unique rapid sleep wakeup feature allows power savings of more than 90% during 'silent' periods. The module may be used in a relaxed sampling mode as long as no movements are detected. RSW also helps saving power, if not the full IF bandwidth of 15kHz is needed.

In battery operated equipment such as traffic control, RSW may significantly lower battery and equipment volume and cost.

#### **RSW in Action**



This graph shows the sampling signal at pin /*Enable* and a resulting output signal at an  $x_AC$  pin caused by an approaching object.

This signal may be processed 'as is' or used as trigger to start continuous acquisition.

If RSW mode is used only to detect any movement, aliasing effects are not important (i.e. undersampling is useful).

By choosing a sampling frequency, aliasing must be taken into account, if frequency measurements are intended.

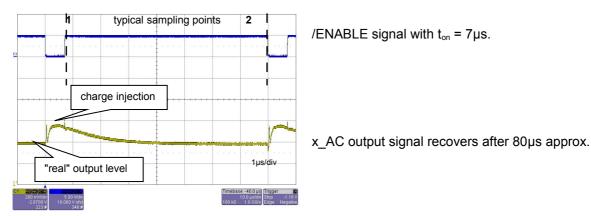
Fig. 7: Sampled Doppler signal at x\_AC outputs

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#### **RSW** principle

RSW combines switching of the RF oscillator and sample&hold of the mixer signals (please refer to Fig. 1: K-MC2 Blockdiagram). During sleep mode (pin /ENABLE = high), only the amplifiers stay switched on to hold the output voltage and coupling capacitor charges. This assures minimum peaks at the outputs when returning to the active state.

Nevertheless, we have to take some important effects into account. An important effect is charge injection, caused by the digital control signal.





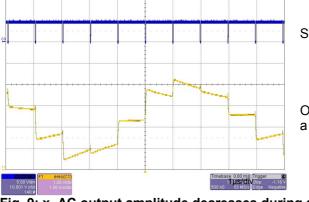
#### Sampling sequence

To simplify signal processing sequence, output sampling may be done immediately after /ENABLE goes high (1) or before next /ENABLE (2).

Both methods have their advantages and disadvantages:

- Sampling point (1) contains a constant overshoot, i.e. sampled output signal becomes shifted by a constant DC component. There is no loss of sensitivity.
- Sampling point (2) corresponds to the real mixer output, as long as sleep time is short enough. But with longer off times, signal amplitude decreases.

As a rule of thumb: with a repeat frequency of 1 kHz (duty cycle of  $7 \mu \text{s}/1\text{ms} = 0.7\%$ ) amplitude loss is 3dB approx. This situation is shown in the figure below.



Sampling signal ( $t_c = 1ms, t_{on} = 7us$ )

Output signal decreases during the off-period with a timeconstant of 4.8ms approx.

Fig. 9: x\_AC output amplitude decreases during sleep time.

#### Sensitivity and Maximum Range

The values indicated here are intended to give you a 'feeling' of the attainable detection range with this module. It is not possible to define an exact RCS (radar cross section) value of real objects because reflectivity depends on many parameters. The RCS variations however influence the maximum range only by  $\sqrt[4]{\sigma}$ .

S:

**f**<sub>0</sub>:

Maximum range for Doppler movement depends mainly on:

- Module sensitivity
- Carrier frequency
- Radar cross section RCS ("reflectivity") of the object  $\sigma^{1}$ :

-145dBc (@1kHz IF Bandwidth)

24.125GHz

1m<sup>2</sup> approx. for a moving person >50m<sup>2</sup> for a moving car

note <sup>1)</sup> RCS indications are very inaccurate and may vary by factors of 10 and more.

The famous "Radar Equation" may be reduced for our K-band module to the following relation:

 $r = 0.0167 \cdot 10^{\frac{-s}{40}} \cdot \sqrt[4]{\sigma}$ 

Using this formula, you get an indicative detection range of

- > 70 meters for a moving person

- > 180 meters for a moving car

Please note, that range values also highly depend on the performance of signal processing, environment conditions (i.e. rain, fog), housing of the module and other factors. Maximal distance is also limited by the phase noise of the oscillator. With K-MC2, you get an absolute maximum range of about 200m.

### **Datasheet Revision History**

Version	Date	Changes	
1.0	10-June-2009	initial release	
1.1	09-Nov-2009	Operating temperature corrected to +80°C	
1.2	17-Dec-2009	VCO tuning range corrected to 90MHz	

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